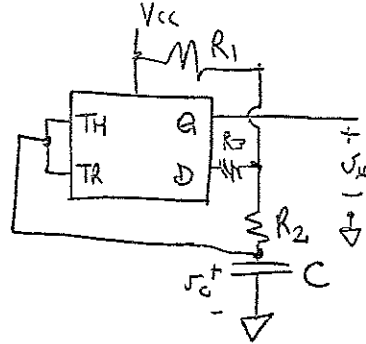


Parte A

1. Si consideri un amplificatore di tensione con  $A_v = 1000$  e polo  $s_p = -100 \text{ rad/s}$ ,  $R_{in} = 2 \text{ M}\Omega$ ,  $R_{out} = 1 \text{ M}\Omega$ . Si reazioni in modo da ottenere un amplificatore con impedenza di ingresso di  $80 \text{ M}\Omega$  e impedenza di uscita maggiore di  $10 \text{ M}\Omega$ . Una volta scelta e dimensionata la rete di reazione, si calcolino le resistenze di ingresso e uscita così ottenute, e il limite superiore di banda del sistema.
2. Disegnare lo schema di un oscillatore di Colpitts e dimensionare i componenti in modo che si inneschi un'oscillazione a frequenza  $2 \text{ MHz}$ . Giustificare il procedimento.
3. Disegnare e quotare la porta complessa CMOS con il minor numero di transistori che svolga la funzione logica  $Y = (\overline{ABC} + AC)$ .
4. Sia dato il circuito a lato, con un timer LM555. Calcolare la forma d'onda generata dal circuito, giustificando il procedimento, e rappresentare la tensione di uscita e la tensione sulla capacità sullo stesso asse dei tempi, quotando i punti rilevanti ( $R_1 = 5 \text{ K}\Omega$ ,  $R_2 = 7 \text{ K}\Omega$ ,  $R_3 = 2 \text{ K}\Omega$ ,  $C = 33 \text{ }\mu\text{F}$ ).



Punteggio totale Parte A: 14

Parte B

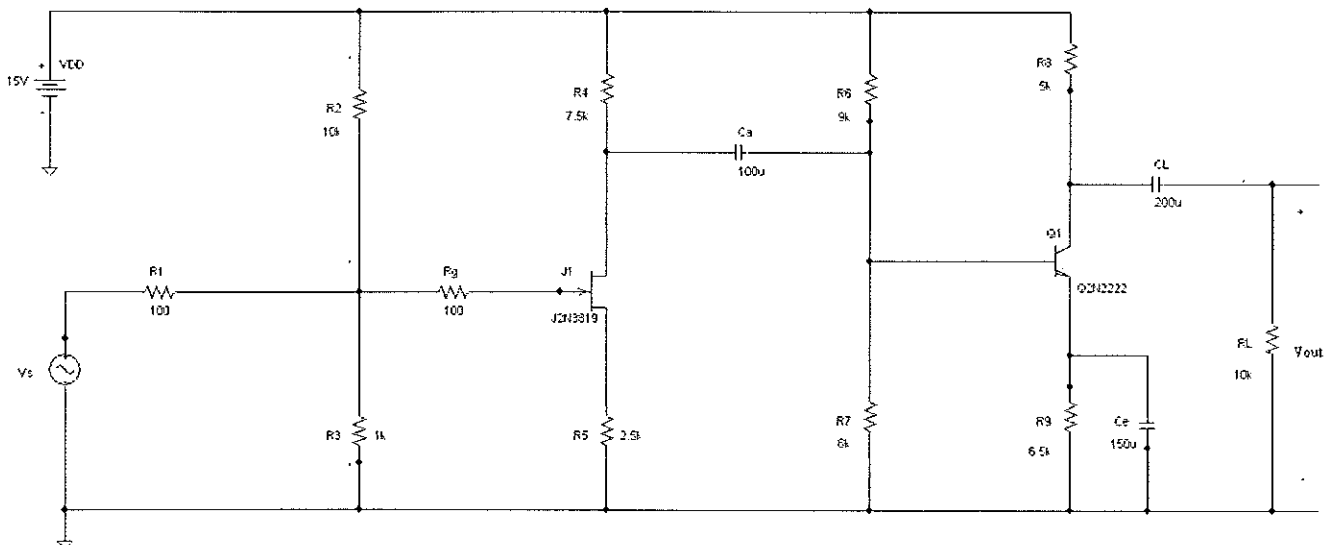
Dato l'amplificatore disegnato in figura, calcolare:

- il punto di riposo dei due transistori,
- l'amplificazione  $V_{out}/V_s$  a centrobanda,
- il limite inferiore di banda e il limite superiore di banda

NOTE:

- Il BJT è un Q2N2222 con  $h_{oe} = 0$ ;
- Il BJT si può considerare resistivo;
- Il JFET è un 2N3819 con  $r_d \rightarrow \infty$

Punteggio totale Parte B: 14.



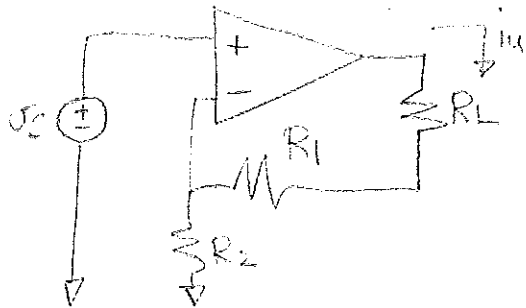
A1

1

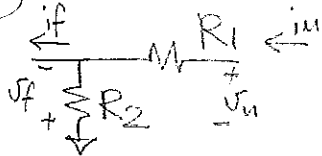
$$R_{in} = 2 M\Omega \rightarrow R_{IF} = 80 M\Omega$$

$$R_{out} = 1 M\Omega \rightarrow R_{OF} > 10 M\Omega$$

Reazione con prelievo di corrente e iniezione di tensione.



rete per  $i_f$

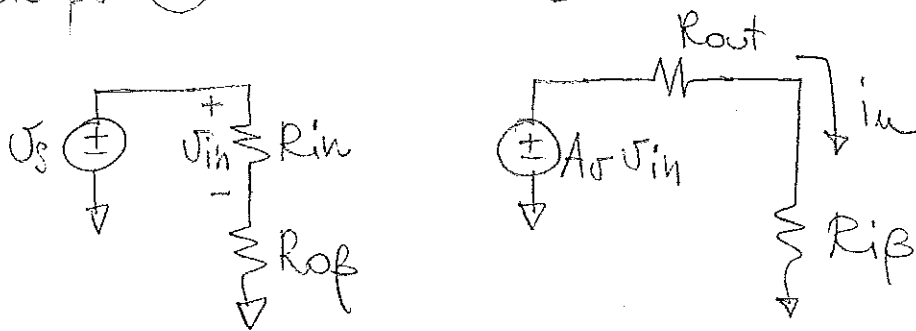


$$i_f = \beta i_u + R_{of} i_f$$

$$v_u = R_{if} i_u + K i_f$$

$$f = \left. \frac{v_f}{i_u} \right|_{i_f=0} = -R_2 ; R_{of\beta} = \left. \frac{v_f}{i_f} \right|_{i_u=0} = R_2 ; R_{if\beta} = \left. \frac{v_u}{i_u} \right|_{i_f=0} = R_1 + R_2$$

rete per  $A_e$  consideriamo  $R_L=0$



$$A_e = \left. \frac{i_u}{v_s} \right|_{\beta=0} = \frac{A_v}{R_{out} + R_{if\beta}} \times \frac{R_{in}}{R_{in} + R_{of\beta}}$$

$$R_{IF} = (R_{in} + R_{of\beta}) (1 - \beta A_e) = 80 M\Omega$$

$$R_{OF} = (R_{if\beta} + R_{out}) (1 - \beta A_e) > 10 M\Omega$$

per soddisfare  $R_{OF}$  è sufficiente che  $(1 - \beta A_e)$  sia  $\gg 10$

RIF per primo:

(2)

poniamo  $R_{of} = R_2 \ll R_{in \text{ last}}$

dobbiamo avere  $1 - \beta A_e = 40 \rightarrow \beta A_e = 39$

$$-\beta A_e = \frac{R_2 A_v}{R_{out} + R_1 + \beta} \cdot \underbrace{\frac{R_{in}}{R_{in} + R_2}}_{\sim 1} = 39$$

scegliamo  $R_1 = 1 \text{ k}\Omega$

$$R_2 A_v = 39 \left( R_{out} - R_1 \right)$$

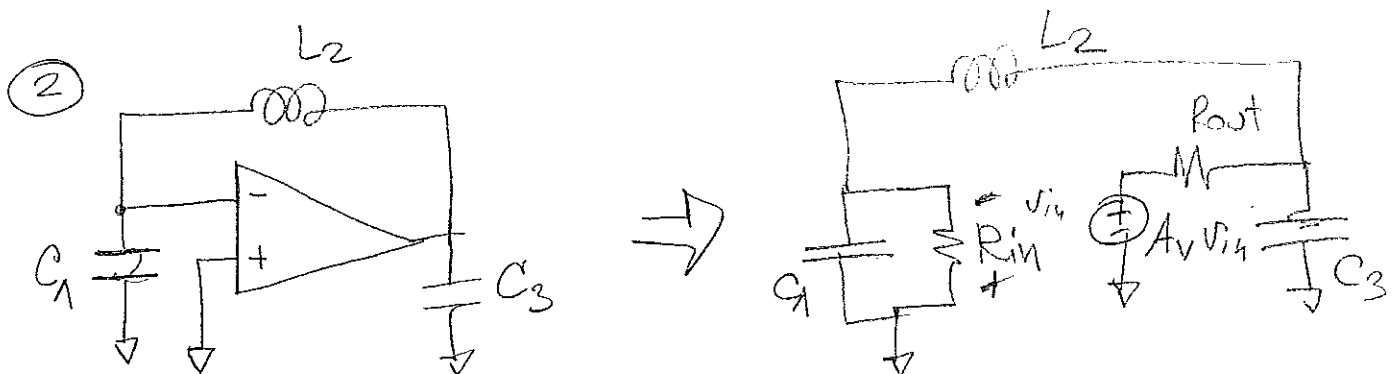
$\uparrow$                      $\uparrow$   
 $1 \text{ M}\Omega$             $1 \text{ k}\Omega$

$$R_2 = \frac{39 \cdot 10^6}{10^3} = 39 \text{ k}\Omega$$

$$R_{IF} = 2.039 \cdot 10^6 \left( 1 + \frac{39 \cdot 10^6}{1.04 \cdot 10^8} \cdot \frac{1 \cdot 10^3}{2.039 \cdot 10^6} \right) = 77,03 \text{ M}\Omega$$

$$R_{OF} = 1.04 \cdot 10^6 \left( 1 + \frac{39 \cdot 2}{1.04 \cdot 2.039} \right) = 59,29 \text{ M}\Omega$$

$$f_H = (1 - \beta A_e) f_p = \frac{100}{2\pi} \left( 1 + \frac{39 \cdot 2}{1.04 \cdot 2.039} \right) = 601 \text{ Hz}$$



$$f_0 = 2 \text{ MHz}$$

poniamo  $R_{in} \Rightarrow 10 \text{ k}\Omega$

dobbiamo avere  $\frac{1}{\omega_0 C_1} \ll R_{in}$

$$C_1 \gg \frac{1}{\omega_0 R_{in}} = \frac{1}{2\pi \cdot 2 \cdot 10^6 \cdot 10 \cdot 10^4} = 0,04 \cdot 10^{-11} = 0,4 \text{ pF}$$

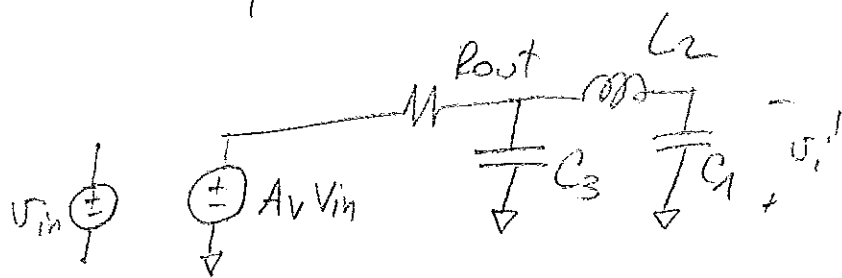
Scegliamo  $C_1 = 10 \text{ pF}$

la frequenza di oscillazione deve essere  $2 \text{ MHz}$

$$\frac{1}{\omega_0 C_1} - \omega_0 L_2 + \frac{1}{\omega_0 C_3} = 0$$

poniamo  $C_3 = C_1 \rightarrow L_2 = \frac{2}{\omega_0^2 C_1} = \frac{2}{(2\pi \cdot 2 \cdot 10^6)^2 \cdot 10^{-11}}$   
 $L_2 = 1,27 \text{ mH}$

infine  $|\beta A(\omega_0)| > 1$

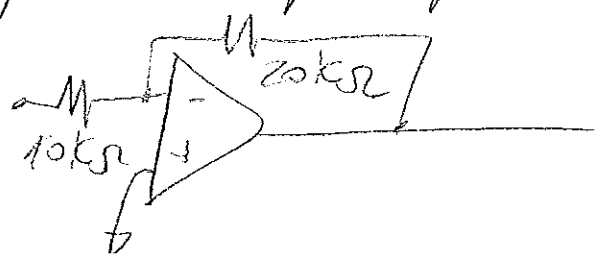


$$\beta A = \frac{v_o'}{v_{in}} = \frac{1}{j\omega_0 C_1} \cdot \frac{1}{j\omega_0 C_3} \cdot \left( \frac{1}{j\omega_0 C_1} + j\omega_0 L_2 \right) A_v$$
~~$$\frac{1}{j\omega_0 C_1} \cdot \frac{1}{j\omega_0 C_3} \cdot \left[ \frac{1}{j\omega_0 C_3} + \frac{1}{j\omega_0 C_1} + j\omega_0 L_2 \right] + \frac{1}{j\omega_0 C_3} \left( \frac{1}{j\omega_0 C_1} + j\omega_0 L_2 \right) A_v$$~~

$$\beta A(\omega_0) = \frac{-A_v}{1 - \omega_0^2 C_1 L_1} = \frac{A_v}{1} \rightarrow \underline{\underline{A_v > 1}}$$

Scegliamo  $A_v > 2$

Come amplificatore buffer per esempio usavo un invertente

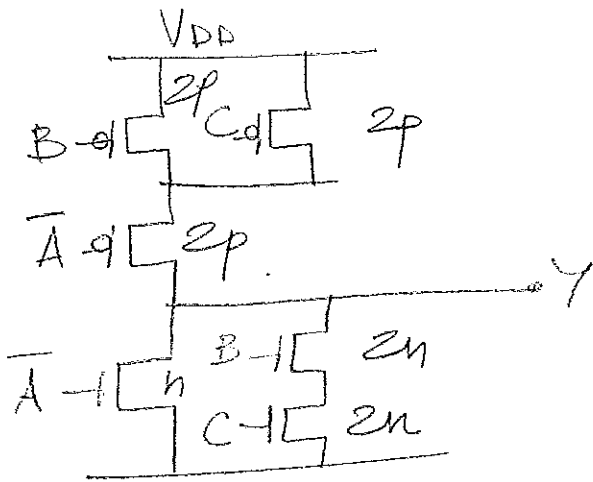


3)

	00	01	11	10
0	0	0	1	1
1	0	0	0	1

$$y = A\bar{C} + A\bar{B} - A(\bar{B} + \bar{C}) \quad (4)$$

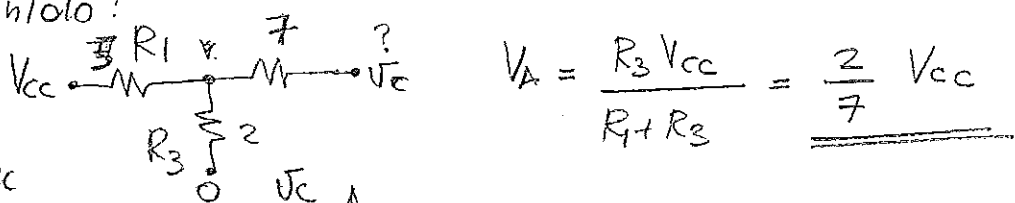
oppure



carica : costante di tempo  $\tau_1 = (R_1 + R_2)C = 12 \cdot 33 \cdot 10^{-3} \text{ s} = 0,396 \text{ s}$   
 da  $\frac{1}{3}V_{cc}$  a  $\frac{2}{3}V_{cc}$

scarica : costante di tempo  $\tau_2 = (R_2 + R_1 \parallel R_3)C =$   
 $= \left(7 + \frac{10}{7}\right) 33 \cdot 10^{-3} = 0,27 \text{ s}$

asintoto:



part=0 sia  $V_c = \frac{1}{3}V_{cc}$

tempo di carica

$$V_c(t) = V_{cc} \left( \frac{1}{3} - \frac{2}{3} e^{-t/\tau_1} \right)$$

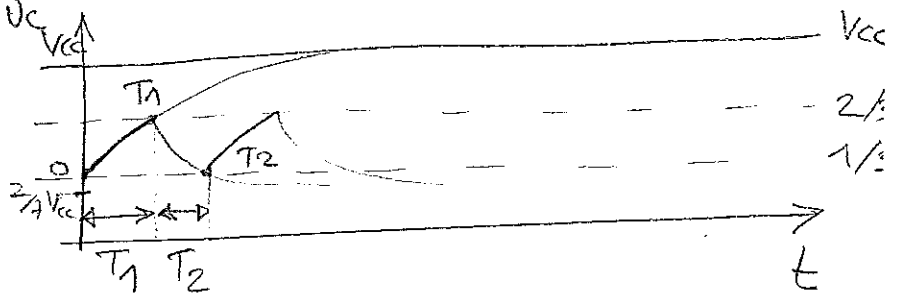
$$V_c(T_1) = \frac{2}{3} V_{cc}$$

$$\frac{2}{3} = 1 - \frac{2}{3} e^{-T_1/\tau_1} \rightarrow T_1 = \tau_1 \ln 2 = 0,274 \text{ s}$$

tempo di scarica

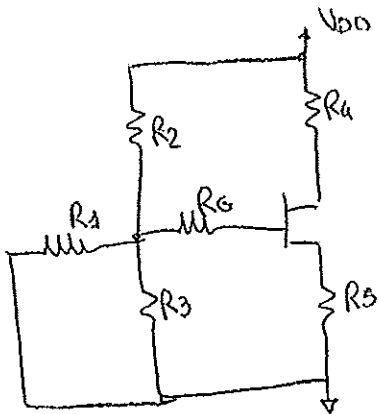
$$V_c(t) = \left( \frac{2}{3} V_{cc} - \frac{2}{7} V_{cc} \right) e^{-\frac{(t-T_1)}{\tau_2}} + \frac{2}{7} V_{cc}$$

$$V_c(T_2) = \frac{1}{3} V_{cc} \rightarrow \frac{1}{3} = \frac{8}{21} e^{-\frac{T_2}{\tau_2}} + \frac{2}{7} = \frac{1}{21} = \frac{8}{21} e^{-\frac{T_2}{\tau_2}} \rightarrow T_2 = \tau_2 \ln 8 = 0,57 \text{ s}$$



PARTE B

PUNTO DI RIPOSO JFET



$$V_G = V_{DD} \cdot \frac{R_1/R_3}{R_1/R_3 + R_2} = 0.835 \text{ V}$$

$$V_{GS} = V_G - R_5 \cdot I_{DS} \Rightarrow I_{DS} = \frac{V_G - V_{GS}}{R_5}$$

DALLE CARATTERISTICHE

$$\begin{cases} V_{GS} = 0 \Rightarrow I_{DS} \approx 0.05 \mu\text{A} \\ V_{GS} = -3 \text{ V} \Rightarrow I_{DS} \approx 1.25 \mu\text{A} \end{cases} \Rightarrow$$

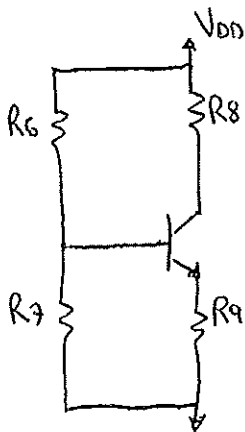
$$\begin{aligned} V_{GS} &\approx -2.165 \text{ V} \\ I_{DS} &\approx 0.92 \mu\text{A} \end{aligned}$$

$$V_{DS} = V_{DD} - (R_4 + R_5) \cdot I_{DS} = 5.8 \text{ V}$$

VERIFICA Hp. JFET IN SATURAZIONE

$$\begin{cases} V_{GS} > V_{GS\text{off}} = -3 \text{ V} \Rightarrow \text{OK} \\ V_{DS} > V_{GS} - V_{GS\text{off}} = 0.835 \Rightarrow \text{OK} \end{cases}$$

PUNTO DI RIPOSO BJT



$$V_B = V_{DD} \cdot \frac{R_7}{R_6 + R_7} = 6 \text{ V}$$

$$V_E = V_B - V_{BE} = 5.3 \text{ V}$$

$$I_C \approx I_E = \frac{V_E}{R_9} = 0.815 \mu\text{A}$$

$$V_{CE} = V_{DD} - (R_8 + R_9) \cdot I_C = 5.628 \text{ V}$$

VERIFICA Hp. PARTITORE PESANTE

$$h_{FE} \approx 150 \text{ DAL GRAFICO}$$

$$I_B \approx \frac{I_C}{h_{FE}} \approx 5.43 \mu\text{A}$$

$$I_{R6} \approx I_{R7} = \frac{V_B}{R_7} = 1 \mu\text{A}$$

$$I_B \ll I_{R6}, I_{R7} \Rightarrow \text{OK}$$

6

PARAMETRI DI PICCOLO SEGNALE JFET

$$g_m \cong 2.5 \text{ mS}$$

$$C_{iss} \cong 2 \text{ pF}$$

$$C_{rss} \cong 0.9 \text{ pF}$$

$$C_{gd} = C_{rss} = 0.9 \text{ pF}$$

$$C_{gs} = C_{iss} - C_{rss} = 1.1 \text{ pF}$$

PARAMETRI DI PICCOLO SEGNALE BJT

$$r_{fe} = \frac{50 + 300}{2} = 175$$

$$r_{ie} @ 1 \text{ mA} = \frac{2 + 8}{2} = 5 \text{ k}\Omega$$

$$r_{b'e} @ 1 \text{ mA} = \frac{V_T \cdot r_{fe}}{I_c @ 1 \text{ mA}} = 4.55 \text{ k}\Omega$$

$$r_{bb'} = r_{ie} - r_{b'e} = 450 \Omega$$

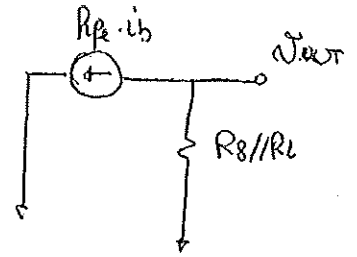
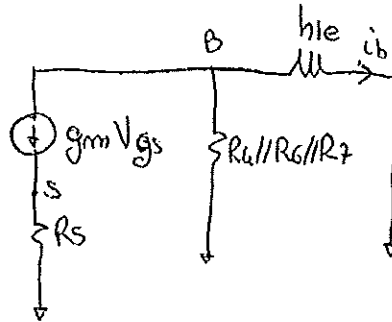
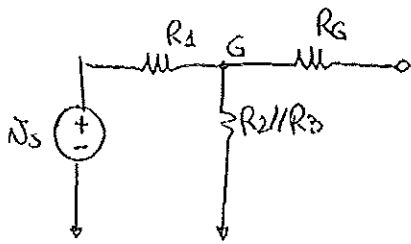
$$r_{b'e} = \frac{V_T \cdot r_{fe}}{I_c} = 5.58 \text{ k}\Omega$$

$$r_{ie} = r_{b'e} + r_{bb'} = 6.03 \text{ k}\Omega$$

$$f_T \cong 80 \text{ MHz}$$

GUADAGNO A CENTRO BANDA

(7)



$$V_{out} = -R_8 // R_L \cdot R_{pe} \cdot i_b$$

$$i_b = -g_m v_{gs} \cdot \frac{R_4 // R_6 // R_7}{R_4 // R_6 // R_7 + h_{ie}}$$

$$v_{gs} = v_s \cdot \frac{R_2 // R_3}{R_2 // R_3 + R_1}$$

$$v_s = R_5 \cdot g_m \cdot v_{gs}$$

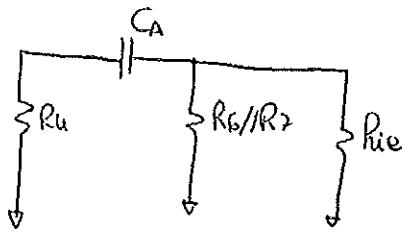
$$v_{gs} = v_s \cdot \frac{R_2 // R_3}{R_2 // R_3 + R_1} - R_5 g_m v_{gs}$$

$$v_{gs} = \frac{1}{1 + R_5 g_m} \cdot \frac{R_2 // R_3}{R_2 // R_3 + R_1} \cdot v_s$$

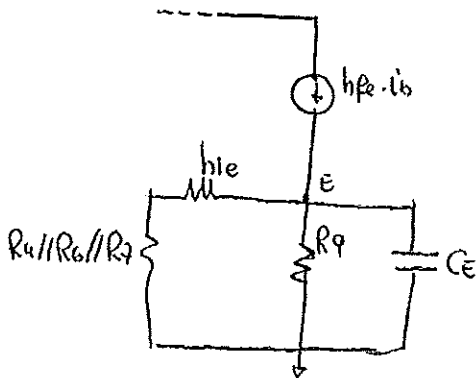
$$A_{co} = \frac{V_{out}}{v_s} = R_8 // R_L \cdot R_{pe} \cdot g_m \cdot \frac{R_4 // R_6 // R_7}{R_4 // R_6 // R_7 + h_{ie}} \cdot \frac{1}{1 + R_5 g_m} \cdot \frac{R_2 // R_3}{R_2 // R_3 + R_1} \cong 5.2$$



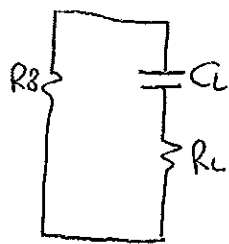
LIMITE INFERIORE DI BANDA



$$R_{VCA} = R_u + R_6 // R_7 // h_{ie} = 9.75 \text{ k}\Omega$$



$$R_{VCE} = R_9 // \left[ \frac{h_{ie} + R_u // R_6 // R_7}{h_{\beta} + 1} \right] \cong 47.6 \Omega$$

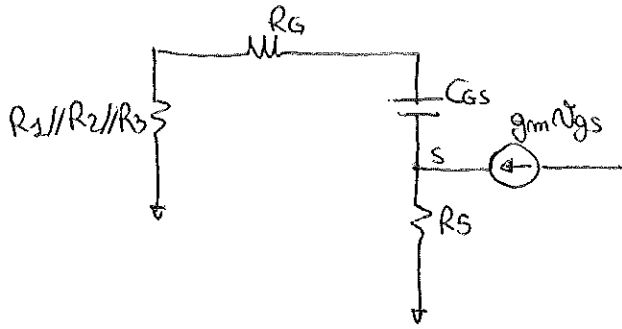


$$R_{VCL} = R_8 + R_L = 15 \text{ k}\Omega$$

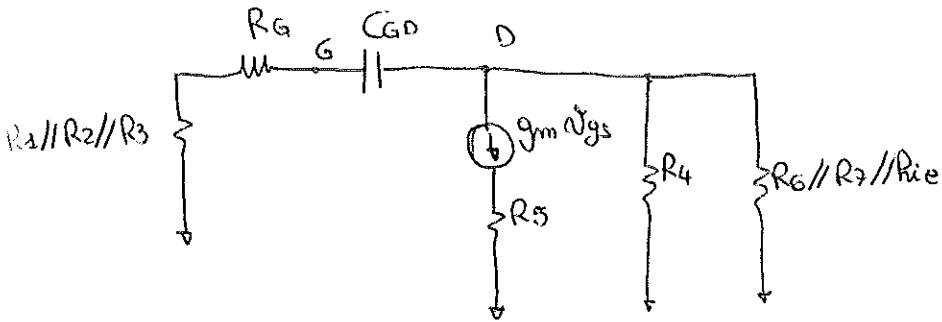
$$f_L = \frac{1}{2\pi} \left[ \frac{1}{R_{VCA} \cdot C_A} + \frac{1}{R_{VCE} \cdot C_E} + \frac{1}{R_{VCL} \cdot C_L} \right] \cong 22 \text{ Hz}$$

LIMITE SUPERIORE DI BANDA

9



$$R_{VGS} = (R_5 + R_G + R_1 // R_2 // R_3) / (1 + g_m R_5) = 371 \Omega$$



$$R_{VGD} = R_4 // R_6 // R_7 // h_{ie} + (R_1 // R_2 // R_3 + R_G) \left[ 1 + \frac{g_m (R_4 // R_6 // R_7 // h_{ie})}{1 + g_m R_5} \right] \cong$$

$$\cong 2.035 \Omega$$

$$f_H = \frac{1}{2\pi (C_{GS} \cdot R_{VGS} + C_{GD} \cdot R_{VGD})} \cong 71 \text{ MHz}$$