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Transmission media characteristics – Optical fibre cables

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**Characteristics of a single-mode optical fibre  
cable**

ITU-T Recommendation G.652

(Formerly CCITT Recommendation)

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### **Characteristics of a single-mode optical fibre cable**

#### **Summary**

This Recommendation describes the geometrical and transmission attributes of single-mode optical fibre and cable with chromatic dispersion and cut-off wavelength that are not shifted from the 1 310 nm wavelength region. Definitions and test methods are contained in a separate ITU-T G.650. Tables of recommended values for different sub-categories of this fibre type are provided to allow ease of reference with regard to the type of system that is supported. Sub-categories described in the tables may differ for technological aspects or for the intended application. Allowed ranges are recommended for both fibre and cable attributes. Information for link attributes and system design is found in Appendix I.

#### **Source**

ITU-T Recommendation G.652 was revised by ITU-T Study Group 15 (1997-2000) and approved by the World Telecommunication Standardization Assembly (Montreal, September 27 – October 6, 2000).

## FOREWORD

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## Recommendation G.652

### Characteristics of a single-mode optical fibre cable

#### 1 Scope

This Recommendation describes a single-mode optical fibre cable which has the zero-dispersion wavelength around 1 310 nm and which is optimized for use in the 1 310 nm wavelength region, and which can also be used in the 1 550 nm region (where this fibre is not optimized). Both analogue and digital transmission can be used with this fibre.

The geometrical, optical, transmission and mechanical parameters are described below in three categories of attributes:

- fibre attributes are those attributes that are retained throughout cabling and installation;
- cable attributes that are recommended for cables as they are delivered;
- link attributes that are characteristic of concatenated cables, describing estimation methods of system interface parameters based on measurements, modelling, or other considerations. Information for link attributes and system design are in Appendix I.

Three tables of recommended values are provided to allow ease of reference. The first table indicates the base subcategory of the optical fibre and cable – appropriate for use with ITU-T G.957 [5] applications. The second contains the values and attributes that are recommended for higher bit rate systems such as those found in ITU-T G.691 [3] and ITU-T G.692 [4]. The third contains values that allow extending ITU-T G.957 [5] transmissions to wavelengths greater than 1 360 nm.

NOTE – Depending on the length of the links, dispersion accommodation can be necessary for some ITU-T G.691 [3] or ITU-T G.692 [4] application codes.

The meaning of the terms used in this Recommendation and the guidelines to be followed in the measurement to verify the various characteristics are given in ITU-T G.650 [1]. The characteristics of this fibre, including the definitions of the relevant parameters, their test methods and relevant values, will be refined as studies and experience progress.

#### 2 References

The following ITU-T Recommendations and other references contain provisions which, through reference in this text, constitute provisions of this Recommendation. At the time of publication, the editions indicated were valid. All Recommendations and other references are subject to revision; all users of this Recommendation are therefore encouraged to investigate the possibility of applying the most recent edition of the Recommendation and other references listed below. A list of the currently valid ITU-T Recommendations is regularly published.

##### 2.1 Normative reference

The following ITU-T Recommendation contains provisions which, through reference in this text, constitute provisions of this Recommendation.

- [1] ITU-T G.650 (2000), *Definition and test methods for the relevant parameters of single-mode fibres*.

## 2.2 Informative references

The following ITU-T Recommendations contain provisions which, through reference in this text, constitute other relevant information.

- [2] ITU-T G.663 (2000), *Application related aspects of optical amplifier devices and subsystems*.
- [3] ITU-T G.691 (2000), *Optical interfaces for single-channel STM-64, STM-256 and other SDH systems with optical amplifiers*.
- [4] ITU-T G.692 (1998), *Optical interfaces for multichannel systems with optical amplifiers*.
- [5] ITU-T G.957 (1999), *Optical interfaces for equipments and systems relating to the synchronous digital hierarchy*.

## 3 Terms and definitions

For the purpose of this Recommendation, the definitions given in ITU-T G.650 [1] apply. Values shall be rounded to the number of digits given in the Tables of Recommended values before conformance is evaluated.

## 4 Abbreviations

This Recommendation uses the following abbreviations:

$A_{\text{eff}}$	Effective Area
DGD	Differential Group Delay
DWDM	Dense Wavelength Division Multiplexing
GPa	GigaPascal
$n_2/A_{\text{eff}}$	Non-linear coefficient
PMD	Polarization Mode Dispersion
SDH	Synchronous Digital Hierarchy
TBD	To Be Determined
WDM	Wavelength Division Multiplexing

## 5 Fibre attributes

Only those characteristics of the fibre providing a minimum essential design framework for fibre manufacture are recommended in this clause. Ranges or limits on values are presented in the tables of clause 7. Of these, cable manufacture or installation may significantly affect the cabled fibre cut-off wavelength and PMD. Otherwise, the recommended characteristics will apply equally to individual fibres, fibres incorporated into a cable wound on a drum, and fibres in an installed cable.

### 5.1 Mode field diameter

Both a nominal value and tolerance about that nominal value shall be specified at 1 310 nm. The nominal that is specified shall be within the range found in clause 7. The specified tolerance shall not exceed the value in clause 7. The deviation from nominal shall not exceed the specified tolerance.

## 5.2 Cladding diameter

The recommended nominal value of the cladding diameter is 125  $\mu\text{m}$ . A tolerance is also specified and shall not exceed the value in clause 7. The cladding deviation from nominal shall not exceed the specified tolerance.

## 5.3 Core concentricity error

The core concentricity error shall not exceed the value specified in clause 7.

## 5.4 Non-circularity

### 5.4.1 Mode field non-circularity

In practice, the mode field non-circularity of fibres having nominally circular mode fields is found to be sufficiently low that propagation and jointing are not affected. It is therefore not considered necessary to recommend a particular value for the mode field non-circularity. It is not normally necessary to measure the mode field non-circularity for acceptance purposes.

### 5.4.2 Cladding non-circularity

The cladding non-circularity shall not exceed the value found in clause 7.

## 5.5 Cut-off wavelength

Three useful types of cut-off wavelength can be distinguished:

- a) cable cut-off wavelength  $\lambda_{cc}$ ;
- b) fibre cut-off wavelength  $\lambda_c$ ;
- c) jumper cable cut-off wavelength  $\lambda_{cj}$ .

NOTE – For some specific submarine cable applications other cable cut-off wavelength values may be required.

The correlation of the measured values of  $\lambda_c$ ,  $\lambda_{cc}$  and  $\lambda_{cj}$  depends on the specific fibre and cable design and the test conditions. While in general  $\lambda_{cc} < \lambda_{cj} < \lambda_c$ , a general quantitative relationship cannot be easily established. The importance of ensuring singlemode transmission in the minimum cable length between joints at the minimum operating wavelength is paramount. This may be performed by recommending the maximum cable cut-off wavelength  $\lambda_{cc}$  of a cabled single-mode fibre to be 1 260 nm, or for typical jumpers by recommending a maximum jumper cable cut-off to be 1 250 nm, or for worst case length and bends by recommending a maximum fibre cut-off wavelength to be 1 250 nm.

The cable cut-off wavelength,  $\lambda_{cc}$ , shall be less than the maximum specified in clause 7.

## 5.6 Macrobanding loss

Macrobanding loss varies with wavelength, bend radius and number of turns about a mandrel with a specified radius. Macrobanding loss shall not exceed the maximum given in clause 7 for the specified wavelength(s), bend radius, and number of turns.

If the fibre is to be used at wavelengths exceeding 1 550 nm, the maximum loss at the highest anticipated wavelength may be projected from a loss measurement at 1 550 nm, using either spectral loss modelling or a statistical data base for that particular fibre design. Alternatively, a qualification test at the longer wavelength may be performed.

NOTE 1 – A qualification test may be sufficient to ensure that this requirement is being met.

NOTE 2 – The recommended number of turns corresponds to the approximate number of turns deployed in all splice cases of a typical repeater span. The recommended radius is equivalent to the minimum bend-radius widely accepted for long-term deployment of fibres in practical systems installations to avoid static-fatigue failure.

NOTE 3 – If for practical reasons fewer than the recommended number of turns are chosen to implement, it is suggested that not less than 40 turns, and a proportionately smaller loss increase be required.

NOTE 4 – If bending radii smaller than the recommended value are planned to be used in splice cases or elsewhere in the system (for example  $R = 30$  mm), it is suggested that the same maximum loss value shall apply to the same number of turns of fibre deployed with this smaller radius.

NOTE 5 – The macrobending loss recommendation relates to the deployment of fibres in practical single-mode fibre installations. The influence of the stranding-related bending radii of cabled single-mode fibres on the loss performance is included in the loss specification of the cabled fibre.

NOTE 6 – In the event that routine tests are required a smaller diameter loop with one or several turns can be used instead of the recommended test, for accuracy and measurement ease. In this case, the loop diameter, number of turns, and the maximum permissible bend loss for the several-turn test should be chosen so as to correlate with the recommended test and allowed loss.

## **5.7 Material properties of the fibre**

### **5.7.1 Fibre materials**

The substances of which the fibres are made should be indicated.

NOTE – Care may be needed in fusion splicing fibres of different substances. Provisional results indicate that adequate splice loss and strength can be achieved when splicing different high-silica fibres.

### **5.7.2 Protective materials**

The physical and chemical properties of the material used for the fibre primary coating and the best way of removing it (if necessary) should be indicated. In the case of single jacketed fibre similar indications shall be given.

### **5.7.3 Proofstress level**

The specified proofstress  $\sigma_p$  shall not be less than the minimum specified in clause 7.

NOTE – The definitions of the mechanical parameters are contained in 1.2 and 2.6/G.650 [1].

## **5.8 Refractive index profile**

The refractive index profile of the fibre does not generally need to be known.

## **5.9 Longitudinal uniformity of chromatic dispersion**

Under study.

NOTE – At a particular wavelength, the local absolute value of the chromatic dispersion coefficient can vary away from the value measured on a long length. If the value decreases to a small value at a wavelength that is close to an operating wavelength in a WDM system, four-wave mixing can induce the propagation of power at other wavelengths, including, but not limited to other operating wavelengths. The magnitude of the four-wave mixing power is a function of the absolute value of the chromatic dispersion coefficient, the chromatic dispersion slope, the operating wavelengths, the optical power, and the distance over which four-wave mixing occurs.

For DWDM operations in the 1 550 nm region, the chromatic dispersion of ITU-T G.652 fibres is large enough to avoid four-wave mixing. Chromatic dispersion uniformity is therefore not a functional issue.

## 5.10 Chromatic dispersion coefficient

The chromatic dispersion coefficient,  $D$ , is specified by putting limits on the parameters of a chromatic dispersion curve that is a function of wavelength in the 1 310 nm region. The chromatic dispersion coefficient limit for any wavelength,  $\lambda$ , is calculated with the minimum zero-dispersion wavelength,  $\lambda_{0\min}$ , the maximum zero-dispersion wavelength,  $\lambda_{0\max}$ , and the maximum zero-dispersion slope coefficient,  $S_{0\max}$ , according to:

$$\frac{\lambda S_{0\max}}{4} \left[ 1 - \left( \frac{\lambda_{0\max}}{\lambda} \right)^4 \right] \leq D(\lambda) \leq \frac{\lambda S_{0\max}}{4} \left[ 1 - \left( \frac{\lambda_{0\min}}{\lambda} \right)^4 \right]$$

The values of  $\lambda_{0\min}$ ,  $\lambda_{0\max}$ , and  $S_{0\max}$  shall be within the ranges specified in clause 7. The above equation, when used with these values, can be used to determine upper limits of the chromatic dispersion coefficient in the 1 550 nm region.

NOTE – It is not necessary to measure the chromatic dispersion coefficient of single-mode fibre on a routine basis.

## 6 Cable attributes

Since the geometrical and optical characteristics of fibres given in clause 5 are barely affected by the cabling process, this clause gives recommendations mainly relevant to transmission characteristics of cabled factory lengths.

Environmental and test conditions are paramount and are described in the guidelines for test methods.

### 6.1 Attenuation coefficient

The attenuation coefficient is specified with a maximum value at one or more wavelengths in both the 1 310 nm and 1 550 nm regions. The optical fibre cable attenuation coefficient values shall not exceed the values found in clause 7.

NOTE – The attenuation coefficient may be calculated across a spectrum of wavelengths, based on measurements at a few (3 to 4) predictor wavelengths. This procedure is described in Appendix II and an example is given in Appendix III.

### 6.2 Polarization mode dispersion coefficient

Not all tables include requirements on PMD. When required, cabled fibre polarization mode dispersion shall be specified on a statistical basis, not on an individual fibre basis. The requirements pertain only to the aspect of the link calculated from cable information. The metrics of the statistical specification are found below. Methods of calculations are found in IEC 61282-3 [B.1], and are summarized in Appendix IV.

The manufacturer shall supply a PMD link design value,  $PMD_Q$ , that serves as a statistical upper bound for the PMD coefficient of the concatenated optical fibre cables within a defined possible link of  $M$  cable sections. The upper bound is defined in terms of a small probability level,  $Q$ , which is the probability that a concatenated PMD coefficient value exceeds  $PMD_Q$ . For the values of  $M$  and  $Q$  given in clause 7, the value of  $PMD_Q$  shall not exceed the maximum PMD coefficient specified in clause 7.

Measurements on uncabled fibre can be used to generate cabled fibre statistics when the design and processes are stable and the relationships between the PMD coefficients of uncabled and cabled fibres are known. When such a relationship has been demonstrated, then the cabler may optionally specify a maximum PMD value on the uncabled fibres.

The limits on the distribution of PMD coefficient values can be interpreted as being nearly equivalent to limits on the statistical variation of the differential group delay (DGD), that varies randomly with time and wavelength. When the PMD coefficient distribution is specified for optical fibre cable, equivalent limits on the variation of DGD can be determined. The metrics and values for link DGD distribution limits are found in Appendix I.

## 7 Tables of recommended values

The following tables summarize the recommended values for a number of species of fibres that satisfy the objectives of this Recommendation.

Table 1 contains the recommended attributes and values needed to support applications such as those recommended in ITU-T G.957 [5] and ITU-T G.691 [3] up to STM-16.

Table 2 contains recommended attributes and values needed to support higher bit rate applications, up to STM-64, such as some in ITU-T G.691 [3] and ITU-T G.692. Depending on link length, dispersion accommodation may be necessary

Table 3 allows ITU-T G.957 [5] transmissions in portions of an extended band of from 1 360 nm to 1 530 nm.

**Table 1/G.652 – G.652.A**

The base subcategory for a single-mode optical fibre cable – suitable for the transmission systems in ITU-T G.957 [5] and ITU-T G.691 [3] up to STM-16.		
Fibre attributes		
Attribute	Detail	Value
Mode field diameter	Wavelength	1 310 nm
	Range of nominal values	8.6-9.5 $\mu\text{m}$
	Tolerance	$\pm 0.7 \mu\text{m}$
Cladding Diameter	Nominal	125.0 $\mu\text{m}$
	Tolerance	$\pm 1 \mu\text{m}$
Core concentricity error	Maximum	0.8 $\mu\text{m}$
Cladding noncircularity	Maximum	2.0%
Cable cut-off wavelength	Maximum	1 260
Macrobend loss	Radius	37.5 mm
	Number of turns	100
	Maximum at 1 550 nm	0.50 dB
Proof stress	Minimum	0.69 GPa
Chromatic dispersion coefficient	$\lambda_{0\text{min}}$	1 300 nm
	$\lambda_{0\text{max}}$	1 324 nm
	$S_{0\text{max}}$	0.093 ps/nm <sup>2</sup> ·km
Cable attributes		
Attribute	Detail	Value
Attenuation coefficient	Wavelength	
	Maximum at 1 310 nm	0.5 dB/km
	Maximum at 1 550 nm	0.4 dB/km

**Table 2/G.652 – G.652.B**

<p>The subcategory for a single-mode optical fibre cable is suitable for the transmission systems in ITU-T G.957 [5], ITU-T G.691 [3] and ITU-T G.692 [4] up to STM-64. Chromatic dispersion will generally need to be accommodated for high bit-rate transmissions in the 1 550 nm wavelength region.</p>		
<b>Fibre attributes</b>		
<b>Attribute</b>	<b>Detail</b>	<b>Value</b>
Mode field diameter	Wavelength	1 310 nm
	Range of nominal values	8.6-9.5 $\mu\text{m}$
	Tolerance	$\pm 0.7 \mu\text{m}$
Cladding Diameter	Nominal	125.0 $\mu\text{m}$
	Tolerance	$\pm 1 \mu\text{m}$
Core concentricity error	Maximum	0.8 $\mu\text{m}$
Cladding noncircularity	Maximum	2.0%
Cable cut-off wavelength	Maximum	1 260 nm
Macrobend loss	Radius	37.5 mm
	Number of turns	100
	Maximum at 1 550 nm	0.50 dB
	Maximum at 16XX nm (Note 1)	0.50 dB
Proof stress	Minimum	0.69 GPa
Chromatic dispersion coefficient	$\lambda_{0\text{min}}$	1 300 nm
	$\lambda_{0\text{max}}$	1 324 nm
	$S_{0\text{max}}$	0.093 ps/nm <sup>2</sup> ·km
Uncabled fibre PMD coefficient	Maximum	ps/ $\sqrt{\text{km}}$ (Note 2)
<b>Cable attributes</b>		
Attenuation coefficient	Maximum at 1 310 nm	0.4 dB/km
	Maximum at 1 550 nm	0.35 dB/km
	Maximum at 16XX nm (Note 1)	0.4 dB/km
PMD coefficient	M	20 cables
	Q	0.01%
	Maximum PMD <sub>Q</sub> (Note 2)	0.5 ps/ $\sqrt{\text{km}}$
<p>NOTE 1 – The upper wavelength of this band has not been fully determined. However, XX is less than or equal to 25 nm.</p> <p>NOTE 2 – An optional maximum PMD coefficient on uncabled fibre may be specified by cabling to support the primary requirement on cable PMD<sub>Q</sub> if it has been demonstrated for a particular cable construction</p>		

**Table 3/G.652 – G.652.C**

<p>The subcategory for a single-mode optical fibre cable is suitable for the transmission systems in ITU-T G.957 [5] and ITU-T G.691 [3] and ITU-T G.692 [4] up to STM-64. Chromatic dispersion will generally need to be accommodated for high bit-rate transmissions in the 1 550 wavelength region. This subcategory also allows ITU-T G.957 [5] transmissions to portions of the band above 1 360 nm and below 1 530 nm. Chromatic dispersion in this extended band may impose requirements on the maximum link length or the need for accommodation.</p>		
<b>Fibre attributes</b>		
<b>Attribute</b>	<b>Detail</b>	<b>Value</b>
Mode field diameter	Wavelength	1 310 nm
	Range of nominal values	8.6-9.5 $\mu\text{m}$
	Tolerance	$\pm 0.7 \mu\text{m}$
Cladding Diameter	Nominal	125.0 $\mu\text{m}$
	Tolerance	$\pm 1 \mu\text{m}$
Core concentricity error	Maximum	0.8 $\mu\text{m}$
Cladding noncircularity	Maximum	2.0%
Cable cut-off wavelength	Maximum	1 260 nm
Macrobend loss	Radius	37.5 mm
	Number of turns	100
	Maximum at 1 550 nm	0.50 dB
	Maximum at 16XX nm (Note 1)	0.50 dB
Proof stress	Minimum	0.69 GPa
Chromatic dispersion coefficient	$\lambda_{0\text{min}}$	1 300 nm
	$\lambda_{0\text{max}}$	1 324 nm
	$S_{0\text{max}}$	0.093 ps/nm <sup>2</sup> ·km
Uncabled fibre PMD coefficient	Maximum	ps/ $\sqrt{\text{km}}$ (Note 2)
<b>Cable attributes</b>		
Attenuation coefficient	Maximum at 1 310 nm	0.4 dB/km
	Maximum at yyyy nm (Note 3)	(Note 4)
	Maximum at 1 550 nm	0.35 dB/km
	Maximum at 16XX nm (Note 1)	0.4 dB/km
PMD coefficient	M	20 cables
	Q	0.01%
	Maximum PMD <sub>Q</sub>	0.5 ps/ $\sqrt{\text{km}}$

**Table 3/G.652 – G.652.C (concluded)**

NOTE 1 – The upper wavelength of this band has not been fully determined. However, XX is less than or equal to 25 nm.

NOTE 2 – An optional maximum PMD coefficient on uncabled fibre may be specified by cabling to support the primary requirement on cable PMD<sub>Q</sub> if it has been demonstrated for a particular cable construction.

NOTE 3 – The wavelength, yyyy, is recommended to be 1 383 nm ≤ yyyy ≤ 1 480 nm, and agreed between buyer and seller. If the water peak (1 383 nm), is specified, then both longer and shorter wavelengths may be used in the extended band. If the specified value is greater than the water peak, then only wavelengths greater than yyyy may be used in the extended band.

NOTE 4 – The sampled attenuation average at yyyy nm shall be less than or equal to the value specified at 1 310 nm after hydrogen ageing according to IEC 60793-2 regarding the B1.3 fibre category (see also Appendix V [B.2]).

## APPENDIX I

### Information for link attributes and system design

A concatenated link usually includes a number of spliced factory lengths of optical fibre cable. The requirements for factory lengths are given in clauses 5 and 6. The transmission parameters for concatenated links must take into account not only the performance of the individual cable lengths but also the statistics of concatenation.

The transmission characteristics of the factory length optical fibre cables will have a certain probability distribution which often needs to be taken into account if the most economic designs are to be obtained. The following paragraphs in this appendix should be read with this statistical nature of the various parameters in mind.

Link attributes are affected by factors other than optical fibre cables by such things as splices, connectors, and installation. These factors cannot be specified in this Recommendation. For the purpose of link attribute values estimation, typical values of optical fibre cables are provided in the tables below. The estimation methods of parameters needed for system design are based on measurements, modelling or other considerations.

#### I.1 Attenuation

The attenuation  $A$  of a link is given by:

$$A = \alpha L + \alpha_s x + \alpha_c y$$

where:

- $\alpha$  typical attenuation coefficient of the fibre cables in a link
- $\alpha_s$  mean splice loss
- $x$  number of splices in a link
- $\alpha_c$  mean loss of line connectors
- $y$  number of line connectors in a link (if provided)
- $L$  Link length

A suitable margin should be allocated for future modifications of cable configurations (additional splices, extra cable lengths, ageing effects, temperature variations, etc.). The above equation does not

include the loss of equipment connectors. The typical values found in I.5 are for the attenuation coefficient of optical fibre cable. The attenuation budget used in designing an actual system should account for the statistical variations in these parameters.

## I.2 Chromatic dispersion

The chromatic dispersion in ps/nm can be calculated from the chromatic dispersion coefficients of the factory lengths, assuming a linear dependence on length, and with due regard for the signs of the coefficients (see 5.10).

When these fibres are used for transmission in the 1 550 nm region, some forms of chromatic dispersion compensation are often employed. In this case, the average link chromatic dispersion is used for design. The measured dispersion in the 1 550 nm window can be characterized within the 1 550 nm window by a linear relationship with wavelength. The relationship is described in terms of the typical chromatic dispersion coefficient and dispersion slope coefficient at 1 550 nm.

Typical values for the chromatic dispersion coefficient,  $D_{1550}$ , and chromatic dispersion slope coefficient,  $S_{1550}$ , at 1 550 nm are found in I.1. These values, together with link length,  $L_{\text{Link}}$ , can be used to calculate the typical chromatic dispersion for use in optical link design.

$$D_{\text{Link}}(\lambda) = L_{\text{Link}} [D_{1550} + S_{1550}(\lambda - 1550)] \quad (\text{ps/nm})$$

## I.3 Differential group delay (DGD)

The differential group delay is the difference in arrival times of the two polarization modes at a particular wavelength and time. For a link with a specific PMD coefficient, the DGD of the link varies randomly with time and wavelength as a Maxwell distribution that contains a single parameter, which is the product of the PMD coefficient of the link and the square root of the link length. The system impairment due to PMD at a specific time and wavelength depends on the DGD at that time and wavelength. So, means of establishing useful limits on the DGD distribution as it relates to the optical fibre cable PMD coefficient distribution and its limits have been developed and are documented in IEC 61282-3 [B.1] and are summarized in Appendix IV. The metrics of the limitations of the DGD distribution follow:

NOTE – The determination of the contribution of components other than optical fibre cable is beyond the scope of this Recommendation, but is discussed in IEC 61282-3 [B.1].

Reference link length,  $L_{\text{Ref}}$ : A maximum link length to which the maximum DGD and probability will apply. For longer link lengths, multiply the maximum DGD by the square root of the ratio of actual length to the reference length.

Typical maximum cable length,  $L_{\text{Cab}}$ : The maxima are assured when the typical individual cables of the concatenation or the lengths of the cables that are measured in determining the PMD coefficient distribution are less than this value.

Maximum DGD,  $DGD_{\text{max}}$ : The DGD value that can be used when considering optical system design.

Maximum probability,  $P_F$ : The probability that an actual DGD value exceeds  $DGD_{\text{max}}$ .

Clause I.5 contains values for these metrics that are appropriate for optical fibre cable that follows the recommended statistical PMD limits in Tables 2 and 3.

## I.4 Nonlinear coefficient

The effect of chromatic dispersion is interactive with the nonlinear coefficient,  $n_2/A_{\text{eff}}$ , regarding system impairments induced by nonlinear optical effects (see ITU-T G.663 [2]). Typical values vary with the implementation. The test methods for nonlinear coefficient remain under study.

## I.5 Tables of common typical values

The values in the following table are representative of concatenated optical fibre cables according to I.1, I.2, and I.3.

Attenuation coefficient	Wavelength region	Typical link value
	1 260 nm-1 360 nm	0.5 dB/km
	1 530 nm-1 565 nm	0.28 dB/km
	1 565 nm-16XX nm (Note 1)	0.35 dB/km
Chromatic dispersion coefficient	$D_{1550}$	17 ps/nm·km
	$S_{1550}$	0.056 ps/nm <sup>2</sup> ·km
Differential group delay (Note 2)	Reference link length	400 km
	Typical maximum cable section length	10 km
	Maximum DGD	25 ps
	Maximum probability	$6.5 \cdot 10^{-8}$
NOTE 1 – The maximum wavelength in this band has not been fully determined. XX, however, is less than or equal to 25 nm.		
NOTE 2 – These values are only appropriate when the cabled PMD <sub>Q</sub> values in Tables 2 and 3 are specified.		

## APPENDIX II

### Spectral Attenuation Modelling

The attenuation coefficient of a fibre across a spectrum of wavelengths may be calculated by means of a characterizing matrix  $M$  and a vector  $v$ . The vector contains the measured attenuation coefficients at a small number (3 to 5) of predictor wavelengths (e.g. 1 300 nm, 1 330 nm, 1 370 nm, 1 380 nm, and/or 1 550 nm). The matrix  $M$  multiplies vector  $v$  to yield another vector  $w$  that predicts the attenuation coefficients at many wavelengths (such as at 10 nm wavelength intervals from 1 240 nm to 1 600 nm).

The matrix  $M$  is given by:

$$\begin{pmatrix} A_{11} & A_{12} & \dots & A_{1n} \\ A_{21} & A_{22} & \dots & A_{2n} \\ \dots & \dots & \dots & \dots \\ A_{m1} & A_{m2} & \dots & A_{mn} \end{pmatrix}$$

where  $m$  is the number of wavelengths where the attenuation coefficients have to be estimated and  $n$  is the number of predictor wavelengths. The matrix  $M$  then multiplies a vector  $v$  ( $n$  elements) containing the measured attenuation coefficients for the specific fibre: the result is a new vector  $w$  ( $m$  elements), giving the estimated values of the attenuation coefficients over the given range, i.e.:

The numerical values in this generic matrix are under consideration. The standard deviation of the difference between the actual and predicted attenuation coefficients is to be better than 0.xx dB/km

in the second window and better than 0.yy dB/km in the third window. The values of xx and yy are under consideration.

Alternatively, the fibre supplier may provide a specific matrix that describes its particular fibre more accurately than the generic matrix. Standard deviations of the difference between actual and predicted values should be quoted. An illustrative example of a specific matrix is presented in Appendix II.

Due to the dependence of the attenuation spectra on the fabrication process, a generic matrix may permit only a rough estimate of the attenuation coefficients. A better approximation can sometimes be obtained by adding another suitable "correction" vector  $e$  to be given by each fibre supplier. Therefore, the estimated attenuation coefficients are the elements of the  $w$  vector:

$$w = M \cdot v + e$$

If the estimate is obtained by using the supplier-specific or fibre type specific matrix  $M$ , then no correction vector  $e$  is necessary.

The elements of both  $M$  and  $e$  are achieved on a statistical basis, so the  $w$  vector elements shall be interpreted as statistical. To indicate the accuracy of the predicted attenuation coefficients, the fibre suppliers shall give a vector containing the standard deviation of the differences between the actual and predicted attenuation coefficients in both windows together with  $M$  and/or  $e$ .

NOTE 1 – In order to facilitate use of this matrix, the fibre should be routinely measured at the predictor wavelengths. The predictor wavelengths should number from 3 to 5, with a strong preference given to the lower number if sufficient accuracy can be achieved. The specific wavelengths (e.g. 1 300 nm, 1 330 nm, 1 370 nm, 1 380 nm, and/or 1 550 nm) are an item for further study.

NOTE 2 – This model considers only uncabled fibre attenuation. An additional vector must be added to  $w$  to take account of cabling effects and environmental effects.

### APPENDIX III

#### **Example of a Matrix Model**

The following is an example of an  $m \times n = 38 \times 3$  matrix. Please note it is given for illustrative purposes only. If the spectral attenuation is to be estimated over the range of 1 240 nm to 1 600 nm (in steps of 10 nm) using 1 310 nm, 1 380 nm, and 1 550 nm as predictor wavelengths, an example of matrix elements which has been shown to be applicable<sup>1</sup> for some ITU-T G.652 fibres follows:

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<sup>1</sup> HANSON (T.A.): Spectral Attenuation Modelling with Matrix Models, *Conference Digest NPL Optical Fibre Measurement Conference (OFMC'91)*, pp. 8-11, York, United Kingdom, 1991.

Output wavelength	Predictive wavelengths		
	( $\mu\text{m}$ )	1 310 nm	1 380 nm
1.23	1.46027	-0.04235	-0.20771
1.24	1.35288	-0.01493	-0.13289
1.25	1.31704	-0.00412	-0.14768
1.26	1.26613	-0.00997	-0.13715
1.27	1.20167	-0.00843	-0.10635
1.28	1.14970	-0.01281	-0.06363
1.29	1.11290	-0.01059	-0.06245
1.30	1.03600	-0.00711	0.00711
1.31	0.96276	0.00342	0.05412
1.32	0.90437	0.01435	0.08572
1.33	0.86168	0.02098	0.11776
1.34	0.83194	0.05500	0.05849
1.35	0.73415	0.08336	0.14196
1.36	0.83266	0.11032	-0.10694
1.37	0.69137	0.22596	-0.05961
1.38	0.01006	0.99798	-0.01126
1.39	-0.25502	0.94764	0.48887
1.40	0.00227	0.58463	0.51813
1.41	0.25780	0.33834	0.40811
1.42	0.29085	0.20419	0.49620
1.43	0.29329	0.13569	0.54995
1.44	0.33133	0.09266	0.51936
1.45	0.31608	0.06343	0.55905
1.46	0.24183	0.04483	0.68361
1.47	0.29207	0.03019	0.59222
1.48	0.19214	0.02196	0.75669
1.49	0.18650	0.01132	0.76122
1.50	0.21242	0.00541	0.70722
1.51	0.16884	0.00648	0.75347
1.52	0.11484	-0.00091	0.84972
1.53	0.09334	0.00419	0.85304
1.54	0.07231	-0.00021	0.88512
1.55	0.03111	-0.00115	0.94957
1.56	0.07054	-0.00321	0.87414
1.57	-0.03723	-0.01127	1.08140
1.58	-0.02543	0.00556	1.01041
1.59	-0.01370	0.00457	0.99389
1.60	-0.06916	-0.00107	1.11623

## APPENDIX IV

### Information on polarization mode dispersion statistics

This appendix is provided to summarize some of the statistical calculations for PMD. IEC 61282-3 [B.1] documents the calculations and theory more completely. This will be given in the following clauses:

IV.1 Introduction

IV.2 Data collection

IV.3 Calculation of  $\text{PMD}_Q$  (Monte Carlo)

IV.4 Calculation for  $\text{DGD}_{\max}$  (Monte Carlo)

NOTE – Other calculation methods are allowed and defined in IEC 61282-3 [B.1]. The Monte Carlo method is given here because it is the easiest to describe.

#### IV.1 Introduction

Polarization mode dispersion (PMD) is a statistical attribute that, for a given fibre, is defined as the average of measured differential group delay (DGD) values across a range of wavelengths. Since the DGD values are random across time and wavelength, there is a theoretical lower limit to achievable reproducibility of the reported PMD value of approximately  $\pm 15\%$ . This feature implies that it is not appropriate to select individual fibres or cables to a specification that is tighter than the capability of the process. Such selections are often appropriate for deterministic attributes like attenuation but are not generally appropriate for PMD. This means that a specification on the overall process distribution is most reasonable.

A second consideration regarding the functionality of PMD is that system impairment at a given time and wavelength is controlled by the DGD value, which varies statistically around the PMD value. If one is given the PMD value for a particular cabled fibre, one can calculate the probability that DGD exceeds a given value. It is clear, however, that application of these formulae to a maximum specified value will yield a very inaccurate view of the actual system performance. A statistical specification on PMD, however, can lead to a statistical boundary on the DGD values for the population as a whole. This boundary, defined in terms of probability, leads to a value for use in system design that is approximately 20% lower in DGD value and two orders of magnitude less in probability than the values that would be obtained without a statistical specification.

From the first consideration, it is desirable to define a single statistical metric for the distribution of the PMD values that are measured on optical fibre cables. The metric therefore must incorporate both aspects of process mean and process variability. An upper confidence limit at some probability level is such a metric.

It is known that the PMD coefficient of a set of concatenated cables can be estimated by the computation of the quadrature average of the PMD coefficients of the individual cables. To give the upper confidence limit metric more meaning in terms of application, the upper bound for a concatenated link of twenty cables is computed. This number of cables is smaller than that used in most links, but is large enough to be meaningful in terms of projecting DGD distributions for concatenated links. A probability value of 0.01% is also standardized – partially on the basis of obtaining equivalence with the probability that DGD exceeds a bound, which is required to be very low. The upper confidence limit is named  $\text{PMD}_Q$ , or link design value and this specification type is known as Method 1.

The probability limit for DGD is set at  $6.5 \cdot 10^{-8}$  based on various system considerations including the presence of other PMD generating components that may be in the links. IEC 61282-3 [B.1] describes a method of determining a maximum (defined in terms of probability) so that if a distribution passes

the Method 1 requirement, the DGD across links comprised of only optical fibre cable will exceed the maximum DGD with a probability less than  $6.5 \cdot 10^{-8}$ . The  $DGD_{max}$  value is established for a broad range of distribution shapes. This  $DGD_{max}$  method of specifying the PMD distribution of optical fibre cables is known as Method 2. Methods of combining the Method 2 parameters with those of other optical components are given in IEC 61282-3 [B.1].

Method 1 is a metric that is based on what is measured and is therefore somewhat more straightforward for use in trade and commerce as a normative requirement. Method 2 is a means of extrapolating the implications for system design and is therefore included as information for system design.

## IV.2 Data collection

The calculations are done with PMD values that are representative of a given cable construction and manufacturing time period. Typically at least 100 values are required. The sample is normally taken on different production cables and different fibre locations within.

The cable distribution can be augmented by measurements of uncabled fibre provided that a stable relationship between uncabled fibre and cable values has been demonstrated for a given construction. One means of such augmentation is to generate several possible cable values from the value of each uncabled fibre. These different values should be selected randomly to represent both the usual relationship and the variability that follows from, for example, measurement reproducibility. Because the range of variations includes reproducibility error, this method of estimating the distribution of cable PMD values can lead to over-estimation of  $PMD_Q$ .

The length of the samples measured could seem to have implications on the Method 2 deductions. This has been studied – with the following conclusions. The Method 2 implications remain valid for any link less than 400 km as long as either:

- the installed cables are less than 10 km; or
- the measured lengths are less than 10 km.

## IV.3 Calculation of $PMD_Q$ (Monte Carlo)

Other methods of calculation are given in IEC 61282-3 [B.1]. The Monte Carlo method is described here because it is the easiest to describe and uses the fewest assumptions.

The measured PMD coefficient values are represented by  $x_i$ , with  $i$  ranging from 1 to  $N$ , the number of measurements. These values will be used to generate 100 000 concatenated link PMD coefficient values, each computed with the quadrature average of 20 individual cable values that are randomly selected from the sample population.

NOTE – when  $N = 100$ , there are  $5.3 \cdot 10^{20}$  possible link values.

For each link value computation, select 20 random numbers between 1 and  $N$ . Select these values and note them with index,  $k$ . The link PMD coefficient,  $y$ , is calculated as:

$$y = \left( \frac{1}{20} \sum_{k=1}^{20} x_k^2 \right)^{1/2} \quad (IV-1)$$

Collect the 100 000 values of  $y$  into a high density histogram as they are being computed. When this computation is complete, calculate the cumulative probability function from the histogram and determine the PMD value associated with the 99.99% level. Report this value as  $PMD_Q$ . If the computed  $PMD_Q$  is less than the specified value (0.5 ps/sqrt(km)), the distribution passes Method 1.

#### IV.4 Calculation for $DGD_{\max}$ (Monte Carlo)

This calculation builds on that of the calculation for  $PMD_Q$ . In this calculation, a value of  $DGD_{\max}$  is predefined (at 25 ps) and a probability of exceeding this value,  $P_F$ , is calculated. If the computed probability is less than the specified value ( $6.5 \cdot 10^{-8}$ ), the distribution passes Method 2.

Before beginning the Monte Carlo, calculate the PMD coefficient limit,  $P_{\max}$ , as:

$$P_{\max} = \frac{DGD_{\max}}{\sqrt{L_{ref}}} = \frac{25}{20} = 1.25$$

For each subsequent pair of 20 cable link concatenation values,  $y_{2j-1}$  and  $y_{2j}$ , a 40 cable concatenation value,  $z_j$ , is generated as:

$$z_j = \left( \frac{y_{2j-1}^2 + y_{2j}^2}{2} \right)^{1/2} \quad (IV-2)$$

NOTE – This yields 50 000 values of  $z_j$ , an adequate number.

Calculate the probability of exceeding  $DGD_{\max}$  on the  $j$ th concatenation of 40 links,  $p_j$ , as

$$p_j = 1 - \int_0^{P_{\max}/z_j} 2 \left( \frac{4}{\pi} \right)^{3/2} \frac{t^2}{\Gamma(3/2)} \exp \left[ -\frac{4}{\pi} t^2 \right] dt \quad (IV-3)$$

Excell<sup>TM</sup> defines a function that can compute  $p_j$ , GAMMADIST (X, ALPHA, BETA, Cumulative). The call to this function should be:

$$PJ = 1 - \text{GAMMADIST}(4 * P_{\max} * P_{\max} / (\pi) * ZI * ZI, 1.5, 1, \text{TRUE}) \quad (IV-4)$$

The probability of exceeding  $DGD_{\max}$ ,  $P_F$ , is given as:

$$P_F = \frac{1}{50000} \sum_j p_j \quad (IV-5)$$

If  $P_F$  is less than the specified value, the distribution passes Method 2.

## APPENDIX V

### Bibliography

- [B.1] IEC 61282-3: work in progress, *Guidelines for the Calculation of PMD in Fibre Optic Systems*.
- [B.2] IEC 60793-2 (86A/563/CDV): work in progress, *Optical fibres – Part 2: Product specifications*.



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